

Effect of Vacuum on Force Response of an Ultrasonic Penetrator

Erin Rezich

NASA Glenn Research Center, Materials and Structures Division,
21000 Brookpark Road, Cleveland, OH 44135; email:

erin.t.rezich@nasa.gov

Jonathan Davis

NASA Glenn Research Center, Propulsion Division, 21000 Brookpark
Road, Cleveland, OH 44135; email: jonathan.k.davis@nasa.gov

Garret Aucutt

New Mexico State University, Department of Civil Engineering, 1780
E University Ave, Las Cruces, NM 88003; email: gma55@nmsu.edu



Background

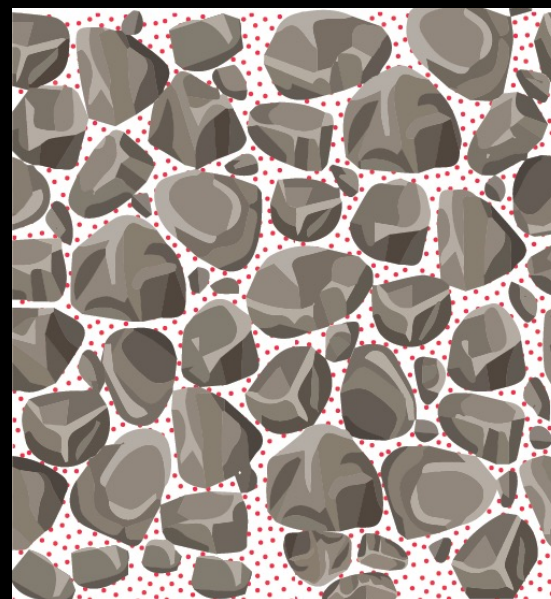
- Previous work has been conducted for simple ultrasonic penetrators in regolith simulants under ambient laboratory conditions and **exhibited significant penetration force reductions** (D. Firstbrook et al., 2017, 2018; D. G. Firstbrook et al., 2014, 2015; Rezich et al., 2021).
- The presence of ambient air is known to affect granular fluidization in that it can impact heaping effects (Pak et al., 1995).
- Multiphase fluidization is also impacted by the development of convective flow patterns (Pak et al., 1995; Valverde, 2015).

Will Vibrofluidization Force Reduction Work on the Moon?

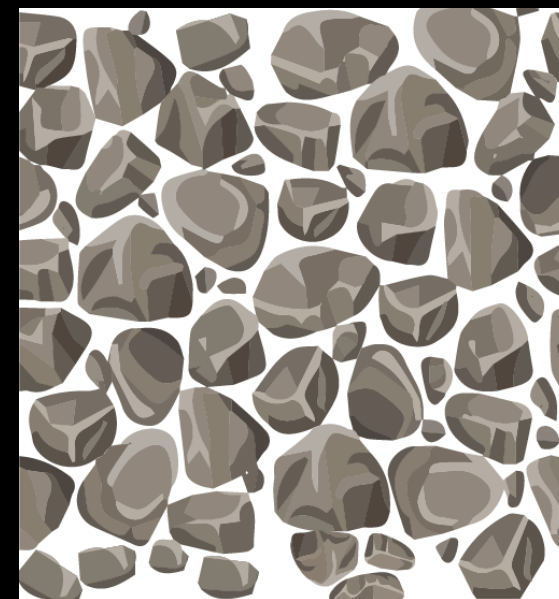
Does interstitial gas (air) within a granular medium (GRC-3 simulant) affect the force response of an ultrasonically vibrating penetrator?

- Does gas assist vibrofluidization via viscous momentum transfer thereby assisting force reduction?
- Does gas damp or dissipate energy transfer to the soil particles thereby reducing force reduction?

Ambient



Vacuum



CUBEvac Test Setup



Figure 1. The CUBEvac experiment setup.
1) Penetration actuation stack,
2) Primary chamber volume where most sensors interface, and
3) Auxiliary chamber volume where the soil bin is located.



Figure 2. Cylinder probe from Sonics and Materials measuring 1.27 cm (0.5 in) in diameter and 5.08 cm (2 in) from the tip to the beginning of the fillet curve.

CUBEvac Sensors and Interfaces

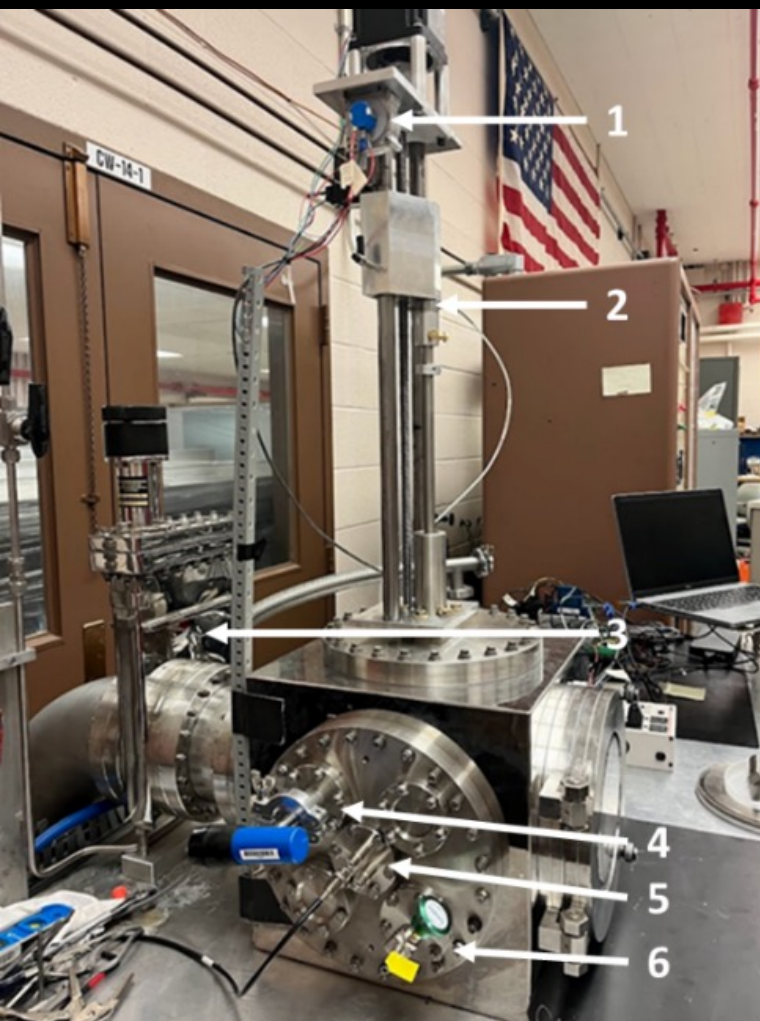


Figure 3. Detailed side views of the CUBEvac test setup.

- 1) String potentiometer,
- 2) in-line, uniaxial tension/compression load cell,
- 3) gate valve to diffusion pump,
- 4) Pirani pressure gauge,
- 5) SHV power connector to ultrasonic piezo transducer,
- 6) chamber vent valve,
- 7) stepper motor used to drive the actuation assembly,
- 8) actuation limit switch,
- 9) combination Pirani and cold cathode pressure gauge,
- 10) chamber roughing valves,
- 11) HEPA filter, and
- 12) line to dry scroll roughing pump.



CUBEvac Stack Cross Section

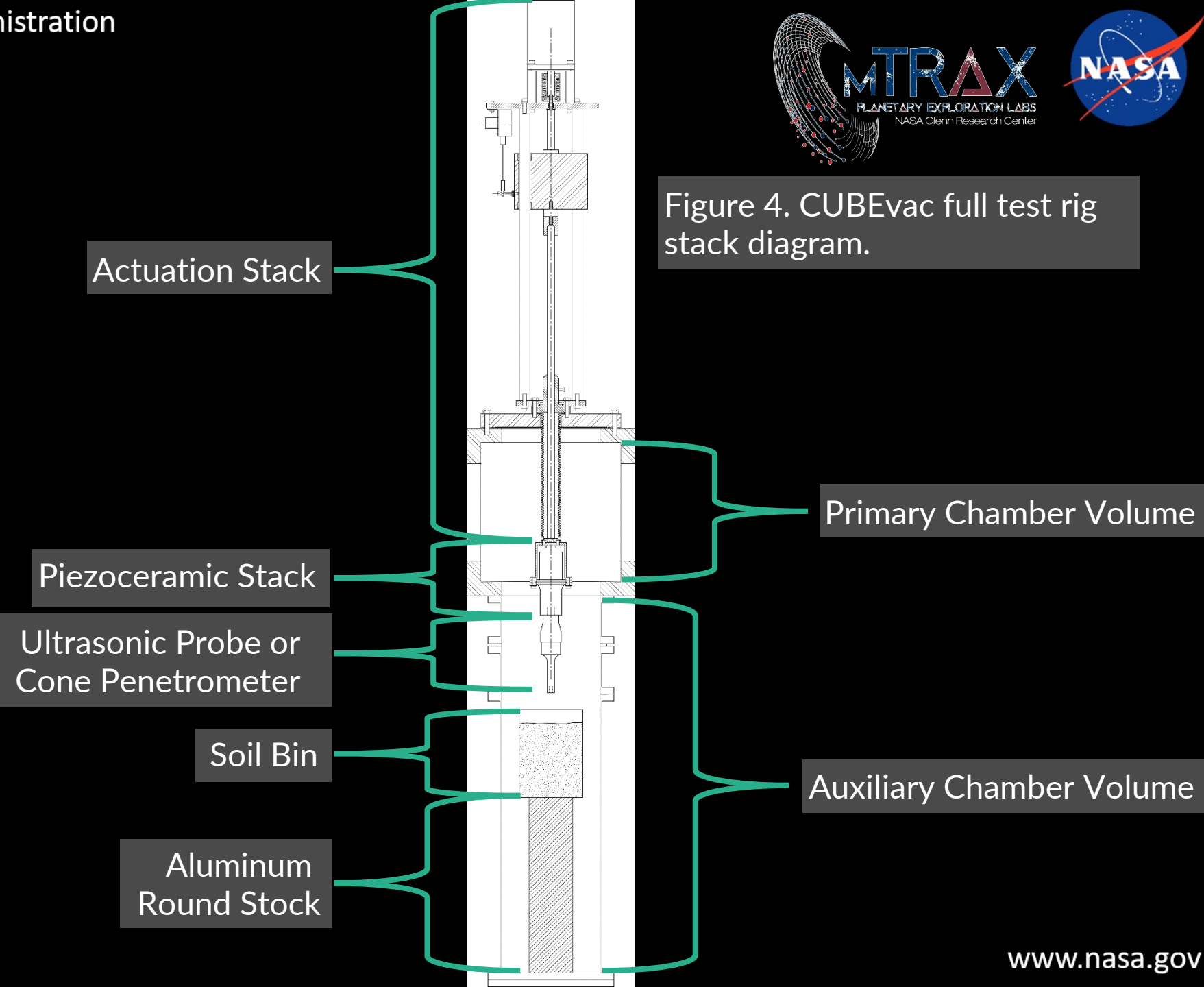


Figure 4. CUBEvac full test rig stack diagram.

Soil Preparation Methodology

1. Start with empty soil bin (steel pot internal diameter of approximately 15.56 cm (6.125 in) and a depth of 19.37 cm (7 5/8 in)
2. Add two scoops of GRC-3 simulant (approximately 0.5 kg) to the bin and tamp down flat. Repeat until soil is 2-3 cm from the top of the bin to allow for a surcharge to be placed on top.
3. Set up soil bin on a 60 Hz vibration table with 34kg surcharge (~ 4 psi) as shown in Figure 5.
4. Vibrate soil for 4 minutes
5. Move soil into chamber and pump down

GRC-3 has a theoretical maximum density of 1.939 g/cm³ (He et al., 2013), and the prepared simulant used in the trials had an estimated bulk density range of 1.895 – 1.934 g/cm³.



Figure 5. Soil preparation vibration table setup with a combined 34 kg of surcharge on the soil surface.

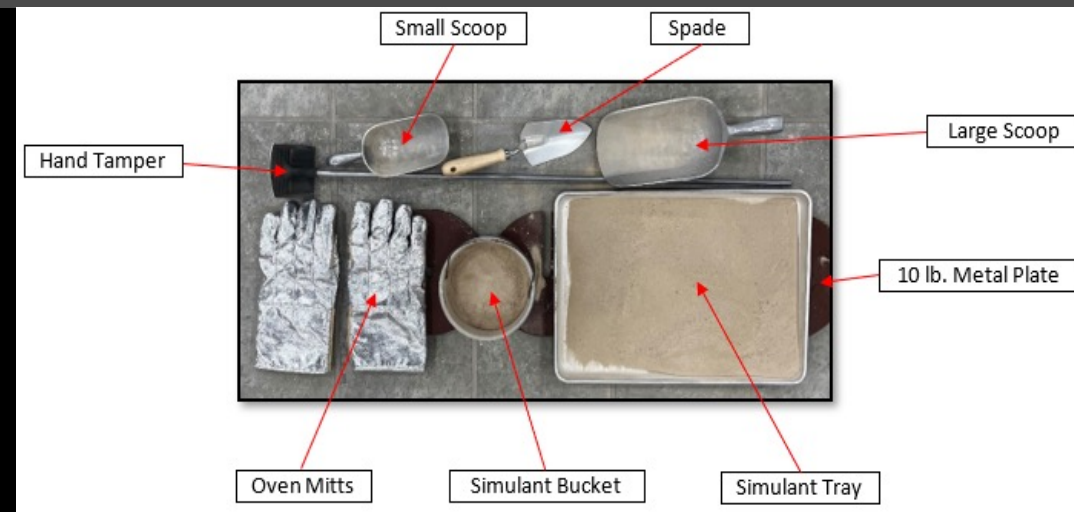
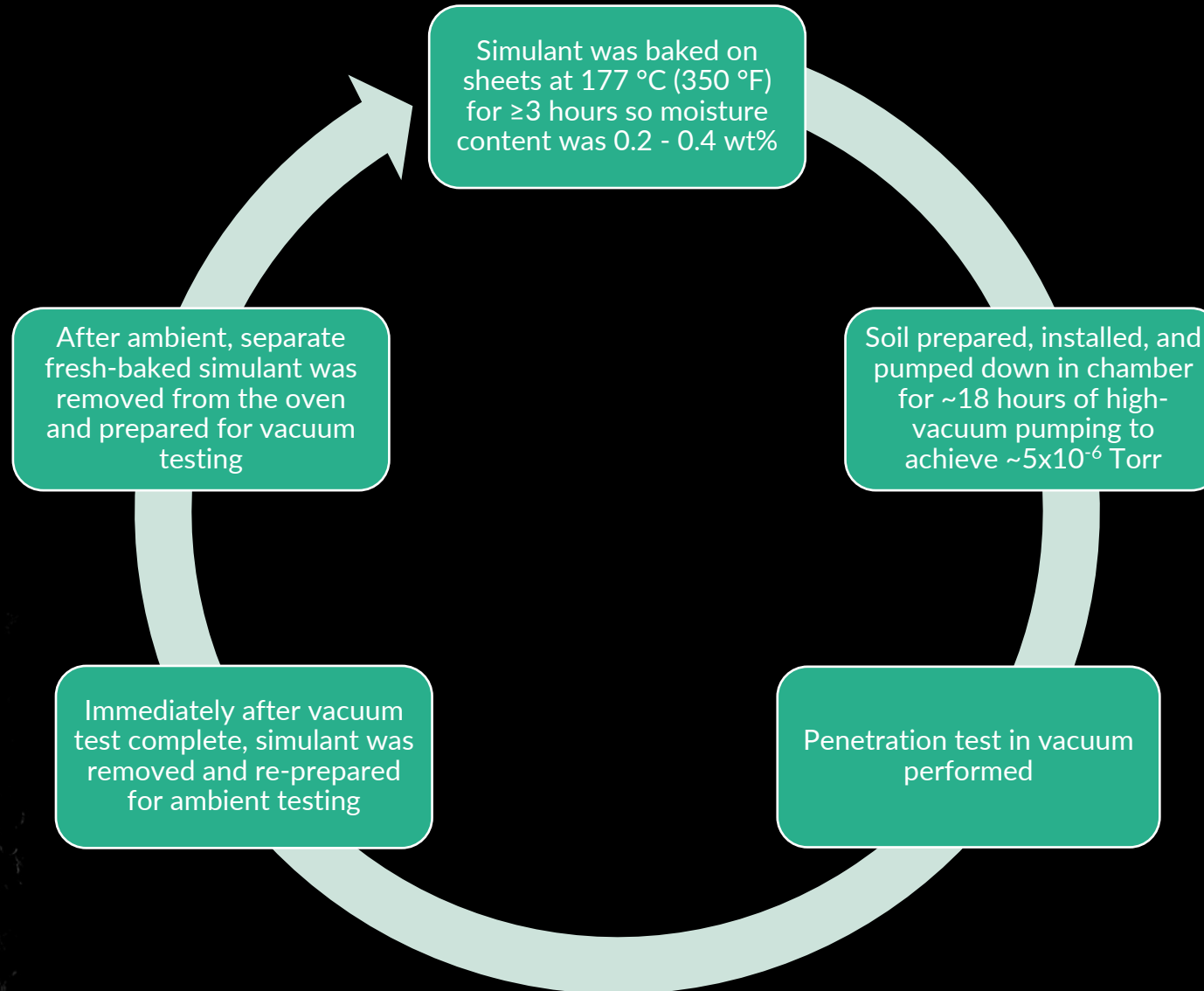


Figure 6. Soil preparation equipment.

Testing Cadence for Moisture Management





Parameters for Cylindrical Probe Tests

Table 1. Test setup parameters for ambient and vacuum environment testing.

	Ambient Environment		Vacuum Environment	
	No Vibration Trials	Active Vibration Trials	No Vibration Trials	Active Vibration Trials
Penetration Speed	2 mm/s	2 mm/s	2 mm/s	2 mm/s
Penetration Depth	50 mm	50 mm	50 mm	50 mm
Vibration Frequency	0 kHz	20 kHz	0 kHz	20 kHz
Vibration Amplitude	0 μm	23 μm	0 μm	23 μm
Chamber Pressure	760 Torr	760 Torr	~5 x 10 ⁻⁶ Torr	~5 x 10 ⁻⁶ Torr



Cone Penetrometer Assessment

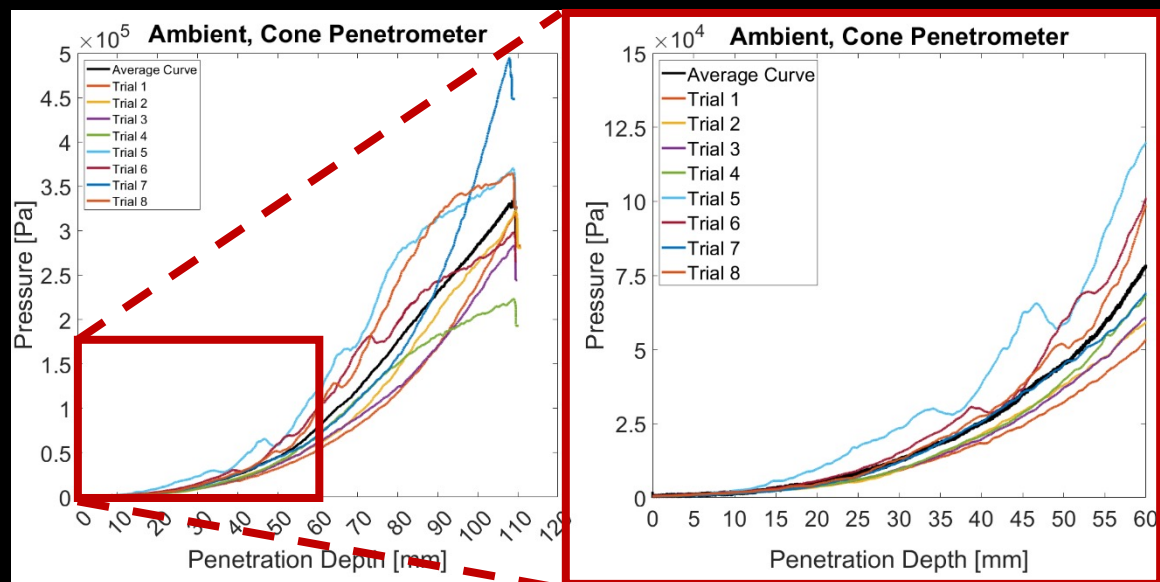


Figure 7. Ambient cone penetration results for full stroke (left) and testing depth only (right).

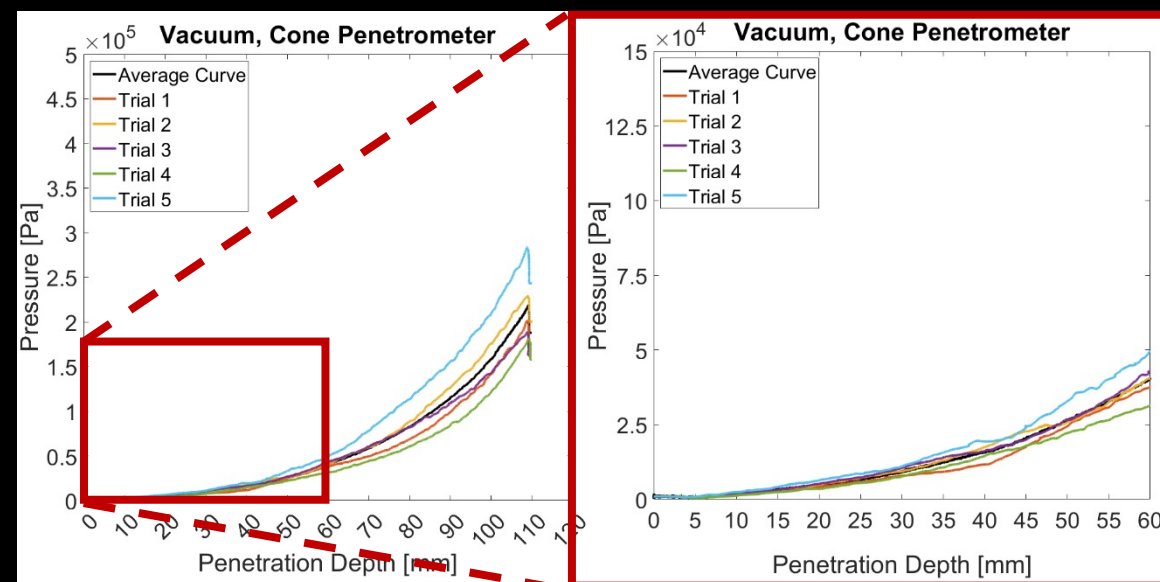


Figure 8. Vacuum cone penetration results for full stroke (left) and testing depth only (right).

NOTE: The cone had a nominal diameter of 12.7 mm (0.5 in) and a nominal height of 28.6 mm (1.125 in)

Ambient soil condition exhibits higher resistance than vacuum soil condition, even to the 50 mm test depth.

Ultrasonic Cylindrical Probe Results - Ambient

Observed advantages of active probe vibration:

- Mitigation of large initial contact force with soil surface
- Highly reduced force variation throughout penetration
- Decreased peak force
- Increased force curve repeatability at current sample size
- Consistently lower force throughout the penetration

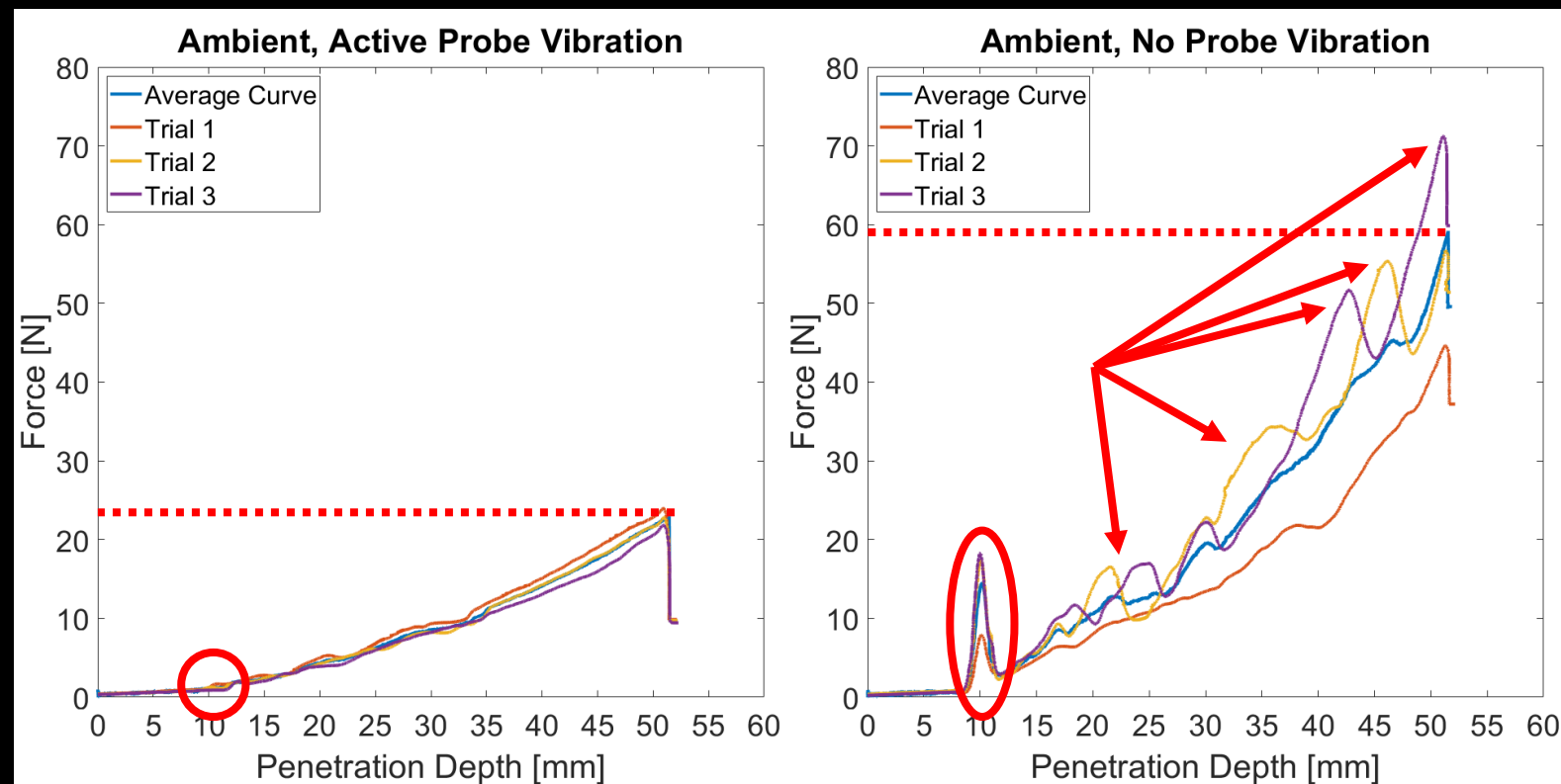


Figure 9. Ambient cylinder penetration trials with active vibration with a 23 μm amplitude (left) and ambient cylinder trials with no active vibration (right).

Ultrasonic Cylindrical Probe Results - Vacuum

Observed advantages of active probe vibration:

- Mitigation of large initial contact force with soil surface
 - NOTE: Soil surface slightly raised in vacuum tests (i.e. contact < 10 mm)
- Highly reduced force variation throughout penetration
- Decreased peak force
- Force curve repeatability not obviously affected at current sample size
- Consistently lower force throughout the penetration

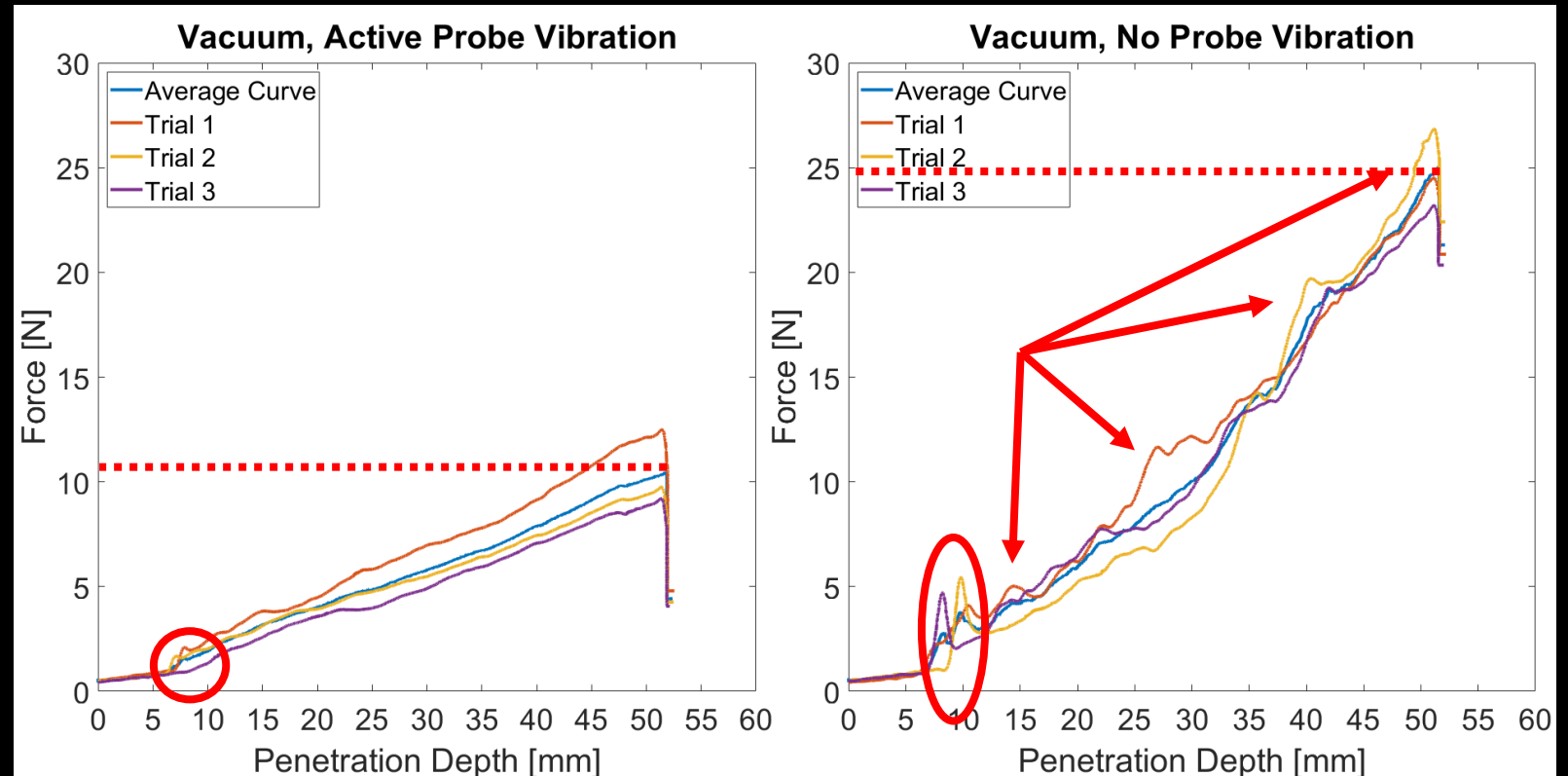


Figure 10. Vacuum cylinder penetration trials with active vibration with a 23 μm amplitude (left) and vacuum cylinder trials with no active vibration (right).

How Much Did the Force Change?

- Y-axis value = ~100%,
implies the forces applied by the probe
with and without active vibration are
equivalent
- Y-axis value > 100%,
force applied with active vibration was
more than without active vibration
- Y-axis value < 100%,
force applied with active vibration was
less than without active vibration

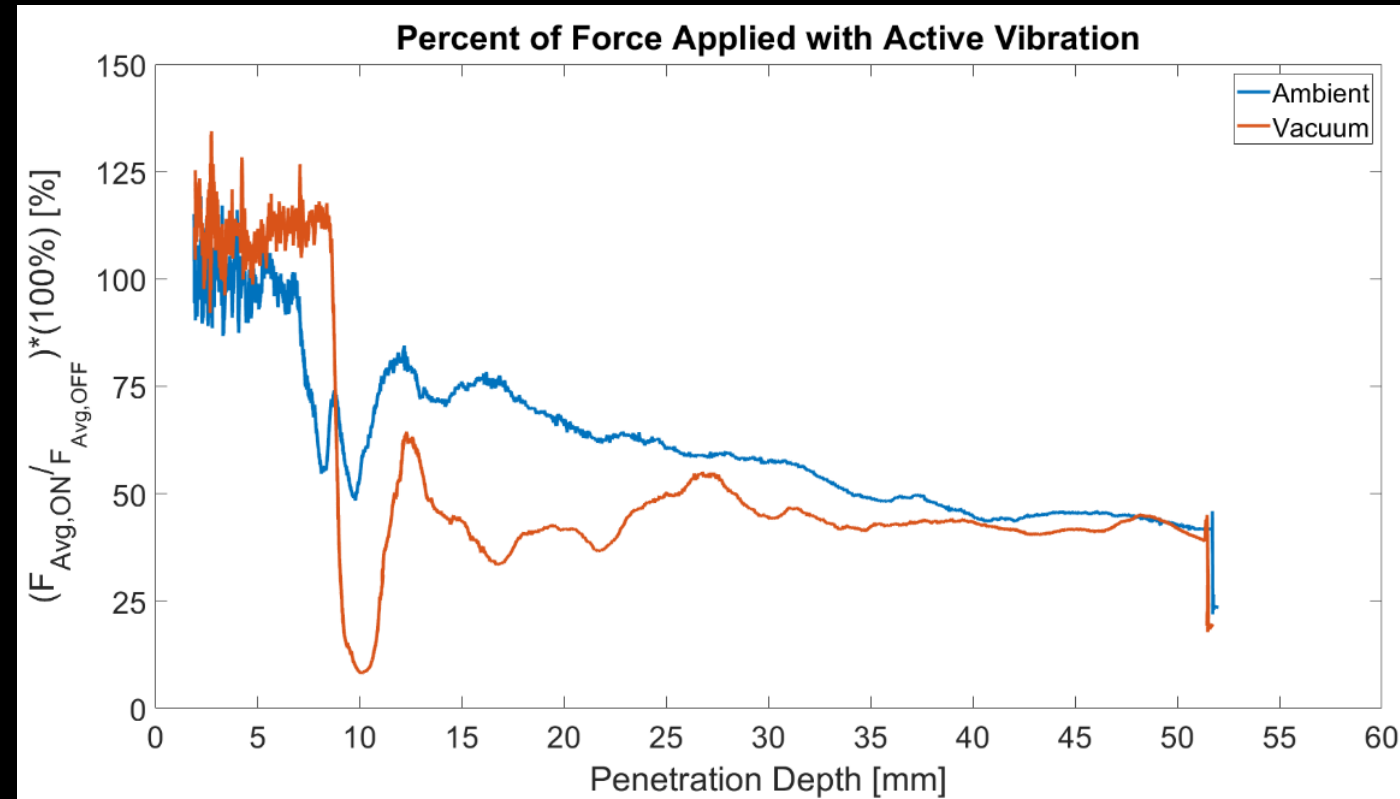


Figure 11. The ratio of penetration force with ultrasonic vibration to penetration force without active vibration in the cylinder probe averaged across repeated trials is shown as a percentage against average penetration depth.



Discussion and Conclusions

- In **ambient** tests, ultrasonic resonant vibration is an effective method of penetration force reduction including more monotonic force response
- In **vacuum** tests, ultrasonic resonant vibration is an effective method of penetration force reduction including more monotonic force response
- A direct comparison of **ambient** and **vacuum** tests is difficult with this dataset due to soil characterization changes in vacuum
 - Soil in-vacuo is inherently drier than the ambient tests. Soil moisture might be causing the measured difference in force response, which can be tested.
- Due to limited trials, it's difficult to confidently say that force reduction due to ultrasonic resonance is **more effective** in a **vacuum** environment as Figure 11 indicates.
- The data does show that the force reduction is **at least as good** in a vacuum environment as it is in ambient testing
 - This indicates that interstitial gas is not required for meaningful force reduction and Figure 11 supports the idea that it acts as an energy dissipation mechanism



Current Path Forward

- Conduct additional testing to better understand the role of interstitial gas in ultrasonic resonance induced vibrofluidization
 - Is force reduction with this method more efficient in vacuum?
- Collect and assess input power data to characterize energy trades between added power requirements and decreased force response
- Develop a theoretical basis to describe vibrofluidized soil motion to assess validity of interstitial gas acting as an energy dissipation mechanism.



References

Firstbrook, D. G., Harkness, P., & Gao, Y. (2014). High-powered ultrasonic penetrators in granular material. AIAA SPACE 2014 Conference and Exposition, September. <https://doi.org/10.2514/6.2014-4265>

Firstbrook, D. G., Harkness, P., & Gao, Y. (2015). Power optimization for an ultrasonic penetrator in granular materials. AIAA SPACE 2015 Conference and Exposition, 1–8. <https://doi.org/10.2514/6.2015-4555>

Firstbrook, D., Worrall, K., Timoney, R., & Harkness, P. (2018). Ultrasonically Assisted Hammer-Action Penetrators in Planetary Regolith. ASCE Earth and Space. <http://eprints.gla.ac.uk/156625/http://eprints.gla.ac.uk>

Firstbrook, D., Worrall, K., Timoney, R., Suñol, F., Gao, Y., & Harkness, P. (2017). An experimental study of ultrasonic vibration and the penetration of granular material. Proceedings of the Royal Society A: Mathematical, Physical and Engineering Sciences, 473. <https://doi.org/10.1098/rspa.2016.0673>

He, C., Zeng, X., & Wilkinson, A. (2013). Geotechnical Properties of GRC-3 Lunar Simulant. *Journal of Aerospace Engineering*, 26(3), 528–534. [https://doi.org/10.1061/\(asce\)as.1943-5525.0000162](https://doi.org/10.1061/(asce)as.1943-5525.0000162)

Pak, H. K., Doom, E. van, & Behringer, R. P. (1995). Effects of Ambient Gases on Granular Materials under Vertical Vibration. 74(23). <https://doi.org/10.+z>

Valverde, J. M. (2015). Convection and fluidization in oscillatory granular flows: The role of acoustic streaming. In *European Physical Journal E* (Vol. 38, Issue 6). Springer New York LLC. <https://doi.org/10.1140/epje/i2015-15066-7>



Questions?

